





```
delta1 = -1*det(mdelta1);
delta2 = det(mdelta2);
delta3 = -1*det(mdelta3);
delta4 = det(mdelta4);
B1 = [beta1 0 0 ; 0 gamma1 0 ; 0 0 delta1 ;
      gamma1 beta1 0 ; 0 delta1 gamma1 ; delta1 0 beta1];
B2 = [beta2 0 0 ; 0 gamma2 0 ; 0 0 delta2 ;
      gamma2 beta2 0 ; 0 delta2 gamma2 ; delta2 0 beta2];
B3 = [beta3 0 0 ; 0 gamma3 0 ; 0 0 delta3 ;
      gamma3 beta3 0 ; 0 delta3 gamma3 ; delta3 0 beta3];
B4 = [beta4 0 0 ; 0 gamma4 0 ; 0 0 delta4 ;
      gamma4 beta4 0 ; 0 delta4 gamma4 ; delta4 0 beta4];
B = [B1 B2 B3 B4]/(6*V);
D = (E/((1+NU)*(1-2*NU)))*[1-NU NU NU 0 0 0 ; NU 1-NU NU 0 0 0 ; NU NU 1-NU 0 0 0 ;
  0 0 0 (1-2*NU)/2 0 0 ; 0 0 0 (1-2*NU)/2 0 ; 0 0 0 0 (1-2*NU)/2];
y = abs(V)*B'*D*B;
%%%%%%%
function y = Tetrahedron3D4Node_Assembly(KK,k,i,j,m,n)
% 该函数进行单元刚度矩阵的组装
% 输入单元刚度矩阵 k
% 输入单元的节点编号 i、j、m、n
% 输出整体刚度矩阵 KK
%
DOF = [3*i-2:3*i,3*j-2:3*j,3*m-2:3*m,3*n-2:3*n];
for n1=1:12
    for n2=1:12
        KK(DOF(n1),DOF(n2))=KK(DOF(n1),DOF(n2))+k(n1,n2);
    end
end
y=KK;
%%%%%%
function y = Tetrahedron3D4Node_Stress(E,NU,x1,y1,z1,x2,y2,z2,x3,y3,z3,x4,y4,z4,u)
% 该函数计算单元的应力
% 输入弹性模量 E, 泊松比 NU
% 输入 4 个节点 i、j、m、n 的坐标 xi,yi,zi,xj,yj,zj,xm,ym,zm,xn,yn,zn
% 输入单元的位移列阵 u(12X1)
% 输出单元的应力 stress(6X1)
% 由于它为常应力单元, 应力分量为 Sx,Sy,Sz,Sxy,Syz,Szx
%
xyz = [1 x1 y1 z1; 1 x2 y2 z2; 1 x3 y3 z3; 1 x4 y4 z4];
V = det(xyz)/6;
mbeta1 = [1 y2 z2; 1 y3 z3; 1 y4 z4];
mbeta2 = [1 y1 z1; 1 y3 z3; 1 y4 z4];
mbeta3 = [1 y1 z1; 1 y2 z2; 1 y4 z4];
mbeta4 = [1 y1 z1; 1 y2 z2; 1 y3 z3];
mgamma1 =[1 x2 z2; 1 x3 z3; 1 x4 z4];
mgamma2 =[1 x1 z1; 1 x3 z3; 1 x4 z4];
mgamma3 =[1 x1 z1; 1 x2 z2; 1 x4 z4];
mgamma4 =[1 x1 z1; 1 x2 z2; 1 x3 z3];
mdelta1 =[1 x2 y2; 1 x3 y3; 1 x4 y4];
mdelta2 =[1 x1 y1; 1 x3 y3; 1 x4 y4];
mdelta3 =[1 x1 y1; 1 x2 y2; 1 x4 y4];
mdelta4 =[1 x1 y1; 1 x2 y2; 1 x3 y3];
beta1 = -1*det(mbeta1);
beta2 = det(mbeta2);
```



```

beta3 = -1*det(mbeta3);
beta4 = det(mbeta4);
gamma1 = det(mgamma1);
gamma2 = -1*det(mgamma2);
gamma3 = det(mgamma3);
gamma4 = -1*det(mgamma4);
delta1 = -1*det(mdelta1);
delta2 = det(mdelta2);
delta3 = -1*det(mdelta3);
delta4 = det(mdelta4);
B1 = [beta1 0 0 ; 0 gamma1 0 ; 0 0 delta1 ;
      gamma1 beta1 0 ; 0 delta1 gamma1 ; delta1 0 beta1];
B2 = [beta2 0 0 ; 0 gamma2 0 ; 0 0 delta2 ;
      gamma2 beta2 0 ; 0 delta2 gamma2 ; delta2 0 beta2];
B3 = [beta3 0 0 ; 0 gamma3 0 ; 0 0 delta3 ;
      gamma3 beta3 0 ; 0 delta3 gamma3 ; delta3 0 beta3];
B4 = [beta4 0 0 ; 0 gamma4 0 ; 0 0 delta4 ;
      gamma4 beta4 0 ; 0 delta4 gamma4 ; delta4 0 beta4];
B = [B1 B2 B3 B4]/(6*V);
D = (E/((1+NU)*(1-2*NU)))*[1-NU NU NU 0 0 0 ; NU 1-NU NU 0 0 0 ; NU NU 1-NU 0 0 0 ;
  0 0 0 (1-2*NU)/2 0 0 ; 0 0 0 0 (1-2*NU)/2 0 ; 0 0 0 0 0 (1-2*NU)/2];
y = D*B*u;
%%%%% Tetrahedron3D4Node %%%% end %%%% %%%

```

**【MATLAB 算例】** 基于 4 节点四面体单元的空间块体分析(Tetrahedron3D4Node)

如图 1 所示的一个块体，在右端面上端点受集中力  $F$  作用。基于 MATLAB 平台，计算各个节点位移、支反力以及单元的应力。取相关参数为：  $E = 1 \times 10^{10} \text{ Pa}$ ,  $\mu = 0.25$ ,

$$F=1\times 10^5 \text{ N}.$$

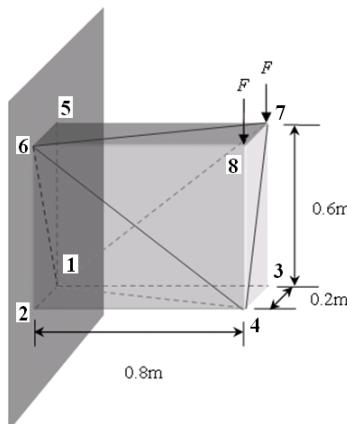


图 1 一个空间块体的分析

**解答：**对该问题进行有限元分析的过程如下。

### (1) 结构的离散化与编号

将结构离散为 5 个 4 节点四面体单元，单元编号及节点编号和坐标如图 4-22 所示，连接关系见表 4-8，节点的坐标见表 4-9。

表 4-8 单元连接关系



单元号	节点号
1	1 4 2 6
2	1 4 3 7
3	6 7 5 1
4	6 7 8 4
5	1 4 6 7

表 4-9 节点的坐标

节点	节点坐标(m)		
	x	y	z
1	0	0	0
2	0.2	0	0
3	0	0.8	0
4	0.2	0.8	0
5	0	0	0.6
6	0.2	0	0.6
7	0	0.8	0.6
8	0.2	0.8	0.6

节点位移列阵

$$\mathbf{q} = [u_1 \quad v_1 \quad w_1 \quad u_2 \quad v_2 \quad w_2 \quad \dots \quad u_8 \quad v_8]^T \quad (4-190)$$

节点外载列阵

$$\mathbf{F} = [0 \quad 0\mathbf{F}_3^T \quad \mathbf{F}_4^T \quad \dots \quad \mathbf{F}_7^T \quad \mathbf{F}_8^T]^T \quad (4-191)$$

其中

$$\mathbf{F}_3 = \mathbf{F}_4 = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix} \quad \mathbf{F}_7 = \mathbf{F}_8 = \begin{bmatrix} 0 \\ 0 \\ -1 \times 10^5 N \end{bmatrix}$$

约束的支反力列阵

$$\mathbf{R} = [\mathbf{R}_1^T \quad \mathbf{R}_2^T \quad 0 \quad 0 \quad \mathbf{R}_5^T \quad \mathbf{R}_6^T \quad 0 \quad 0]^T \quad (4-192)$$

其中

$$\mathbf{R}_1 = \begin{bmatrix} R_{1x} \\ R_{1y} \\ R_{1z} \end{bmatrix} \quad \mathbf{R}_2 = \begin{bmatrix} R_{2x} \\ R_{2y} \\ R_{2z} \end{bmatrix} \quad \mathbf{R}_5 = \begin{bmatrix} R_{5x} \\ R_{5y} \\ R_{5z} \end{bmatrix} \quad \mathbf{R}_6 = \begin{bmatrix} R_{6x} \\ R_{6y} \\ R_{6z} \end{bmatrix}$$

总的节点载荷列阵

$$\mathbf{P} = \mathbf{F} + \mathbf{R} = \mathbf{R} = [\mathbf{R}_1^T \quad \mathbf{R}_2^T \quad \mathbf{F}_3^T \quad \mathbf{F}_4^T \quad \mathbf{R}_5^T \quad \mathbf{R}_6^T \quad \mathbf{F}_7^T \quad \mathbf{F}_8^T]^T \quad (4-193)$$

## (2) 计算各单元的刚度矩阵(以国际标准单位)



首先在 MATLAB 环境下，输入弹性模量 E、泊松比 NU，然后针对单元 1 和单元 2，分别调用 5 次函数 Tetrahedron3D4Node\_Stiffness，就可以得到单元的刚度矩阵  $k1(6 \times 6) \sim k5(6 \times 6)$ 。

```
>> E=1e10;
>> NU=0.25;
>> k1 = Tetrahedron3D4Node_Stiffness(E,NU,0,0,0,0.2,0.8,0,0.2,0,0,0.2,0,0.6);
>> k2 = Tetrahedron3D4Node_Stiffness(E,NU,0,0,0,0.2,0.8,0,0.8,0,0,0.8,0.6);
>> k3 = Tetrahedron3D4Node_Stiffness(E,NU,0.2,0,0.6,0,0.8,0.6,0,0,0.6,0,0,0);
>> k4=Tetrahedron3D4Node_Stiffness(E,NU,0.2,0,0.6,0,0.8,0.6,0.2,0.8,0.6,0.2,0.8,0);
>> k5 = Tetrahedron3D4Node_Stiffness(E,NU,0,0,0,0.2,0.8,0,0.2,0,0.6,0,0.8,0.6);
```

### (3) 建立整体刚度方程

由于该结构共有 8 个节点，则总共的自由度数为 24，因此，结构总的刚度矩阵为  $KK(24 \times 24)$ ，先对  $KK$  清零，然后 5 次调用函数 Tetrahedron3D4Node\_Assembly 进行刚度矩阵的组装。

```
>> KK = zeros(24);
>> KK = Tetrahedron3D4Node_Assembly(KK,k1,1,4,2,6);
>> KK = Tetrahedron3D4Node_Assembly(KK,k2,1,4,3,7);
>> KK = Tetrahedron3D4Node_Assembly(KK,k3,6,7,5,1);
>> KK = Tetrahedron3D4Node_Assembly(KK,k4,6,7,8,4);
>> KK = Tetrahedron3D4Node_Assembly(KK,k5,1,4,6,7);
```

### (4) 边界条件的处理及刚度方程求解

由图 4-22 可以看出，节点 1、2、5、6 上三个方向的位移将为零，即  $u_1 = v_1 = w_1 = u_2 = v_2 = w_2 = u_5 = v_5 = w_5 = u_6 = v_6 = w_6 = 0$ 。因此，将针对节点 3、4、7、8 的位移进行求解，节点 1、2、5、6 的位移将对应  $KK$  矩阵中的第 1 至 6 行，第 13 至 18 行和第 1 至 6 列，第 13 至 18 列，需从  $KK(24 \times 24)$  中提出，置给  $k$ ，然后生成对应的载荷列阵  $p$ ，再采用高斯消去法进行求解，注意：MATLAB 中的反斜线符号“\”就是采用高斯消去法。

```
>>k=KK([7:12,19:24],[7:12,19:24]);
>>p=[0,0,0,0,0,0,-1e5,0,0,-1e5]';
>>u=k\p
u = 1.0e-003 *
    0.1249   -0.0485   -0.4024    0.1343   -0.0715   -0.4031      [将列排成行]
    0.1314    0.0858   -0.4460    0.1353    0.0681   -0.4742      [将列排成行]
```

由此可以看出，所求得的位移结果见表 4-10。

表 4-10 空间块体的节点位移计算结果

$u_3 = 0.1249 \times 10^{-3}$	$u_7 = 0.1314 \times 10^{-3}$
$v_3 = -0.0485 \times 10^{-3}$	$v_7 = 0.0858 \times 10^{-3}$
$w_3 = -0.4024 \times 10^{-3}$	$w_7 = -0.4460 \times 10^{-3}$
$u_4 = 0.1343 \times 10^{-3}$	$u_8 = 0.1353 \times 10^{-3}$
$v_4 = -0.0715 \times 10^{-3}$	$v_8 = 0.0681 \times 10^{-3}$
$w_4 = -0.4031 \times 10^{-3}$	$w_8 = -0.4742 \times 10^{-3}$

### (5) 支反力的计算



在得到整个结构的节点位移后，由原整体刚度方程就可以计算出对应的支反力；先将上面得到的位移结果与位移边界条件的节点位移进行组合(注意位置关系)，可以得到整体的位移列阵  $U(24 \times 1)$ ，再代回原整体刚度方程，计算出所有的节点力  $P(24 \times 1)$ ，按式(4-192)的对应关系就可以找到对应的支反力。

```
>>U=zeros(6,1);u([1:6]);zeros(6,1);u(7:12]);
>>P=KK*U
P = 1.0e+005 *
    0.3372    1.3774    0.1904   -0.4202    1.2892    0.4984    [将列排成行]
   -0.0000    0.0000    0.0000   -0.0000   -0.0000   -0.0000    [将列排成行]
   -0.4745   -1.3774    0.5604    0.5575   -1.2892    0.7509    [将列排成行]
   -0.0000   -0.0000   -1.0000   -0.0000    0.0000   -1.0000    [将列排成行]
```

由式(4-193)的对应关系，可以得到对应的支反力见表 4-11。

表 4-11 空间块体的支反力计算结果

$R_{1x} = 0.3372 \times 10^5 N$	$R_{5x} = -0.4745 \times 10^5 N$
$R_{1y} = 1.3774 \times 10^5 N$	$R_{5y} = -1.3774 \times 10^5 N$
$R_{1z} = 0.1904 \times 10^5 N$	$R_{5z} = 0.5604 \times 10^5 N$
$R_{2x} = -0.4202 \times 10^5 N$	$R_{6x} = 0.5575 \times 10^5 N$
$R_{2y} = 1.2892 \times 10^5 N$	$R_{6y} = -1.2892 \times 10^5 N$
$R_{2z} = 0.4984 \times 10^5 N$	$R_{6z} = 0.7509 \times 10^5 N$

## (6) 各单元的应力计算

先从整体位移列阵  $U(24 \times 1)$  中提取出单元的位移列阵，然后，调用计算单元应力的函数 Tetrahedron3D4Node\_Stress，就可以得到各个单元的应力分量。

```
>>u1=[U(1:3);U(10:12);U(4:6);U(16:18)];
>>stress1=Tetrahedron3D4Node_Stress(E,NU,0,0,0,0.2,0.8,0,0.2,0,0,0.2,0,0.6,u1)
stress1 = 1.0e+006 *
   -0.3574   -1.0721   -0.3574    0.6717   -2.0155      0    [将列排成行]
>>u2=[U(1:3);U(10:12);U(7:9);U(19:21)];
>> stress2=Tetrahedron3D4Node_Stress(E,NU,0,0,0,0.2,0.8,0,0.2,0,0,0.2,0,0.6,u2)
stress2 = 1.0e+006 *
   0.0314   -0.8298   -0.9260    0.1649   -1.1170    0.0294    [将列排成行]
>> u3=[U(16:21);U(13:15);U(1:3)];
>> stress3=Tetrahedron3D4Node_Stress(E,NU,0.2,0,0.6,0,0.8,0.6,0,0.6,0,0,0,u3)
stress3 = 1.0e+006 *
   0.4289    1.2867    0.4289    0.6568   -2.2301      0    [将列排成行]
>> u4=[U(16:21);U(22:24);U(10:12)];
>> stress4=Tetrahedron3D4Node_Stress(E,NU,0.2,0,0.6,0,0.8,0.6,0.2,0.8,0.6,0.2,0.8,0,u4)
stress4 = 1.0e+006 *
   0.1046    0.6272   -1.0012    0.3233   -1.4402   -0.5562    [将列排成行]
>> u5=[U(1:3);U(10:12);U(16:21)];
>> stress5=Tetrahedron3D4Node_Stress(E,NU,0,0,0,0.2,0.8,0,0.2,0,0.6,0,0.8,0.6,u5)
stress5 = 1.0e+006 *
   -0.0179   -0.0060   -0.3636   -0.9083   -1.5986    0.4192    [将列排成行]
```

各个单元应力分量的计算结果列在表 4-12 中。

表 4-12 空间块体的各个单元应力分量的计算结果



1号单元	$\sigma_x = -0.3574 MPa$	$\sigma_y = -1.0721 MPa$	$\sigma_z = -0.3574 MPa$
	$\tau_{xy} = 0.6717 MPa$	$\tau_{yz} = -2.0155 MPa$	$\tau_{zx} = 0 MPa$
2号单元	$\sigma_x = 0.0314 MPa$	$\sigma_y = -0.8298 MPa$	$\sigma_z = -0.9260 MPa$
	$\tau_{xy} = 0.1649 MPa$	$\tau_{yz} = -1.1170 MPa$	$\tau_{zx} = 0.0294 MPa$
3号单元	$\sigma_x = 0.4289 MPa$	$\sigma_y = 1.2867 MPa$	$\sigma_z = 0.4289 MPa$
	$\tau_{xy} = 0.6568 MPa$	$\tau_{yz} = -2.2301 MPa$	$\tau_{zx} = 0 MPa$
4号单元	$\sigma_x = 0.1046 MPa$	$\sigma_y = 0.6272 MPa$	$\sigma_z = -1.0012 MPa$
	$\tau_{xy} = 0.3233 MPa$	$\tau_{yz} = -1.4402 MPa$	$\tau_{zx} = -0.5562 MPa$
5号单元	$\sigma_x = -0.0179 MPa$	$\sigma_y = -0.0060 MPa$	$\sigma_z = -0.3636 MPa$
	$\tau_{xy} = -0.9083 MPa$	$\tau_{yz} = -1.5986 MPa$	$\tau_{zx} = 0.4192 MPa$